

# Azimuthal Anisotropy Measurements in PHENIX via Cumulants of Multi-particle Azimuthal Correlations



the PHENIX Collaboration

#### Anisotropy Measurements via Cumulants

## **Introduction**

High energy-density nuclear matter is believed to be created in heavy ion collisions at RHIC. The statistical and dynamical properties of this matter is of great current interest.

Azimuthal anisotropy ( $v_2$ ) provides an important probe for high energy-density nuclear matter because it is sensitive to early pressure build-up in heavy-ion collisions. The development and dynamic evolution of this pressure is believed to be related to the the equation of state (EOS) and a possible phase transition.

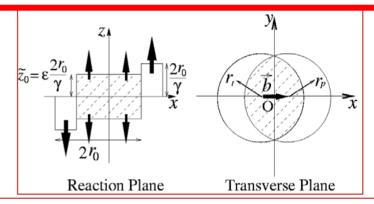


Fig. 1

Schematic view of a nuclear collision in the reaction plane (left) and transverse to the plane (right). Pressure gradients developed in the overlap region can lead to relatively strong momentum anisotropy.

- Detailed measurements of v<sub>2</sub> can:
  - Provide an important probe for the EOS
  - Assist in discriminating between different sources of the anisotropy such as flow and jets
  - Validate and/or constrain models

#### Common Methods for Anisotropy Measurements at RHIC

There are two main techniques which are commonly exploited to make anisotropy measurements at RHIC. Both are influenced by non-harmonic contributions.

#### 1. The reaction plane method:

This method involves an evaluation of the mean anisotropy of particles relative to an inferred reaction plane;

$$\left\langle e^{2i\left(\phi - \phi_R\right)}\right\rangle_{events} = \left\langle cos 2\left(\phi - \phi_R\right)\right\rangle_{events} = v_2$$

 $\phi$ : azimuth of particle  $\phi_p$ : azimuth of reaction plane

Application of a correction factor for reaction plane dispersion is required to obtain accurate anisotropy values.

#### The method of two particle correlation functions:

This method involves an evaluation of the mean anisotropy between particle pairs;

$$\left\langle e^{in\left(\phi_{1}-\phi_{2}\right)}\right\rangle = \left\langle e^{in\left(\phi_{1}-\phi_{R}\right)}\right\rangle \left\langle e^{in\left(\phi_{R}-\phi_{2}\right)}\right\rangle + \left\langle e^{in\left(\phi_{1}-\phi_{2}\right)}\right\rangle_{c}$$

$$= v_{2}^{2} + O\left(\frac{1}{M}\right)$$
 **no correction factor is required**

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#### Cumulant Method (2<sup>nd</sup> order)

## **Analysis Method**

This analysis exploits the cumulant method of **Borghini, Dinh and Ollitrault** (Phys.Rev.C 64 054901 (2001) to make detailed differential measurements of  $v_2$ . That is, flow harmonics are calculated via the cumulants of multiparticle azimuthal correlations and non-flow contributions are removed by higher order cumulants.

Two-particle correlations can be decomposed into a harmonic and a non-harmonic term (hereafter termed flow and non-flow).

measured flow nonflow
$$\left\langle e^{in(\varphi_1 - \varphi_2)} \right\rangle_m = v_n^2 + \left\langle e^{in(\varphi_1 - \varphi_2)} \right\rangle_c$$

Thus, the second order cumulant can be written as;

$$C_2\{2\} = \langle \langle e^{2i(\phi_1 - \phi_2)} \rangle \rangle = v_2^2 + \langle e^{2i(\phi_1 - \phi_2)} \rangle_c(1)$$

and is relatively straightforward to evaluate.

#### Cumulant Method (4th order)

# If flow predominates, cumulants of higher order can be used to reduce non-flow contributions

• Following the decomposition strategy presented earlier for two-particle correlations, the 4 particle correlations can be similarly decomposed as follows:

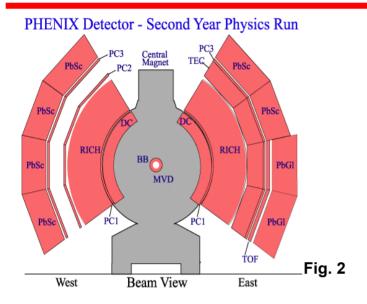
$$C_{n}\left\{4\right\} = \left\langle e^{in(\varphi_{1} + \varphi_{2} - \varphi_{3} - \varphi_{4})} \right\rangle - \left\langle e^{in(\varphi_{1} - \varphi_{2})} \right\rangle \left\langle e^{in(\varphi_{3} - \varphi_{4})} \right\rangle - \left\langle e^{in(\varphi_{3} - \varphi_{4})} \right\rangle \left\langle e^{in(\varphi_{3} - \varphi_{4})} \right\rangle$$

$$\langle \langle e^{2i(\phi_1 - \phi_2 + \phi_3 - \phi_4)} \rangle \rangle \equiv \langle e^{2i(\phi_1 - \phi_2 + \phi_3 - \phi_4)} \rangle - 2\langle e^{2i(\phi_1 - \phi_2)} \rangle^2$$

$$= -v_2^4 + O\left(\frac{1}{M}\right)$$

Improved accuracy is clearly achieved if  $v_2 \gg \frac{1}{M^{\frac{3}{4}}}$ 

#### Data Analysis Procedure (I)



# Cumulant analysis in PHENIX Follows three basic steps.

- I. Track selection
- II. Evaluation of the cumulants
- III. Application of an acceptance correction

#### Track Selection

- Event selection:
  - 22.3 M minimum bias Au+Au (200 GeV) events
- Tracks reconstructed using

Drift Chamber (DC), PadChamber1 (PC1) PadChamber3 (PC3)

#### **Track Selection:**

- Good quality tracks
- 2σ PC3 matching to reduce background
- > Transverse momentum cut:

0.3-2.0 GeV/c for integral 0.3-4.0 GeV/c for differential

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#### Data Analysis Procedure (cumulant generation)

II. Cumulants for the integral and differential flow are generated via generating functions

$$C_2(x,y) = M\left(\langle G_2(x,y)\rangle^{\frac{1}{M}} - 1\right) \qquad D_2(x,y) = \frac{\langle e^{2i\psi}G_2(x,y)\rangle}{\langle G_2(x,y)\rangle}$$

**Integral flow** 

**Differential flow** 

where

$$G_2(x,y) = \prod_{j=1}^{M} \left(1 + \frac{2x\cos 2\phi_j + 2y\sin 2\phi_j}{M}\right)$$

and  $\psi$  is the azimuth of a particle in the  $p_T$  window of interest

- A fixed number (M) of particles is selected at random to generate cumulants for integral flow to avoid errors due to multiplicity fluctuations
- Particles for integral flow chosen outside of the  $(p_T, \eta)$  window of interest to avoid autocorrelations

#### Data Analysis Procedure (acceptance/efficiency correction)

The anisotropy is corrected for acceptance/efficiency via a Fourier series expansion of the PHENIX azimuthal acceptance:

$$A\left(\phi\right) = \sum_{k=-\infty}^{k=+\infty} a_k e^{ik\phi}$$

A non-isotropic acceptance, as in the PHENIX detector, entails a mixing of different harmonics, and hence leads to modified relations between cumulants and flow

For instance, for the 2<sup>nd</sup> order cumulant

$$c_2 \{2\} = v_2^2$$
 for a perfect acceptance

becomes  $c_2$   $\{2\} = k_1 v_1^2 + k_2 v_2^2$  for a non-perfect acceptance where  $k_1$  and  $k_2$  are functions of the Fourier coefficients  $a_k$ 

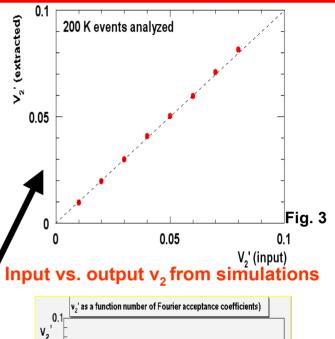
- Similarly  $c_1 \{2\} = k_1 v_1^2 + k_2 v_2^2$
- Combining the equations above gives  $v_2$  in terms of  $c_1\{2\}$  and  $c_2\{2\}$

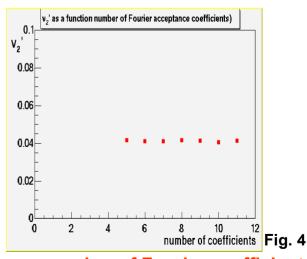
#### Test Demonstration of the Robustness of the Analysis Procedure

A cumulant analysis in PHENIX is non-trivial, primarily because of the relatively limited acceptance of the device. This being the case, it is important to demonstrate the reliability of our extraction procedure.

- Monte Carlo simulation tests were performed with known v<sub>2</sub> and the PHENIX acceptance as input
- Generated events were then analyzed through our analysis framework.
- The results from these tests show that the v<sub>2</sub> extracted is robust and acceptance corrections are very well implemented

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v<sub>2</sub> vs. number of Fourier coefficients used for acceptance correction

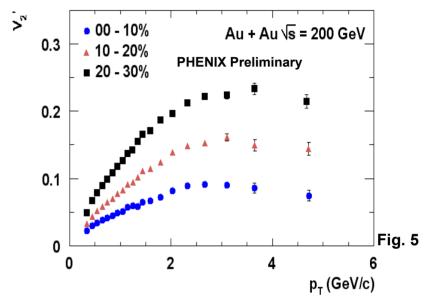
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#### Experimental Results (pT and centrality dependence)

The cumulant method has been used to make very detailed studies of the anisotropy as a function of

- centrality
- pseudo-rapidity
- Transverse momentum (pT)
- pT and centrality
- pT of the particles used to construct integral flow etc..

In the following, several representative results are shown.



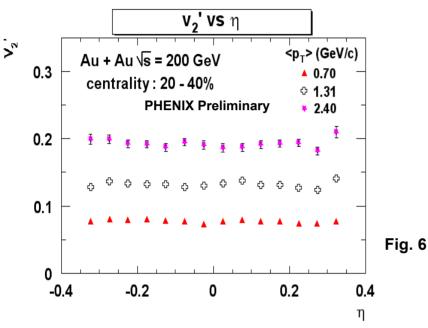
The pT dependence of  $v_2$  show:

- Saturation for pT > 2 GeV/c
- Increases with centrality and pT

High pT particles which are dominantly from jets are clearly correlated with low pT particles which are thought to be associated with softer processes.

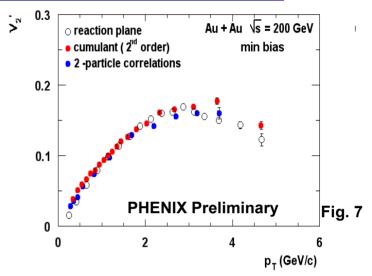
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#### Experimental Results (pseudo-rapidity dependence)



• The pseudo-rapidity dependence of V2 (for several pT selections) is essentially flat within the PHENIX acceptance.

#### Comparison between methods



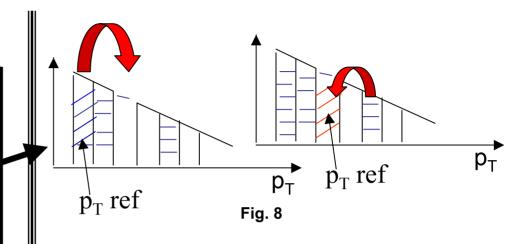
- Relatively good agreement is found between values obtained from second order cumulants and those obtained from the reaction plane and two particle correlation function methods.
- Small deviations for pT > 3 GeV/c may be due to an increase in the influence of jets.

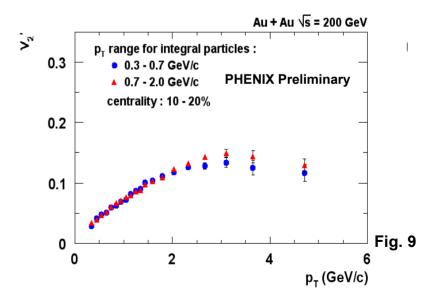
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#### Experimental Results (dependence on pT of the Reference)

Given the fact that soft processes are expected to dominate at low pT and harder processes at higher pT, v<sub>2</sub> was extracted for several different pT reference

- No significant dependence on the p<sub>T</sub> of reference is observed for pT < 2 Gev/c</li>
- For pT > 2.5 GeV/c, the trend is compatible with an increase in the jet contribution to the anisotropy.





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#### Experimental Results (Centrality dependence)

Anisotropy can result from hydrolike flow and jet-quenching. In both of these cases, the initial eccentricity is a major driving force for the anisotropy.

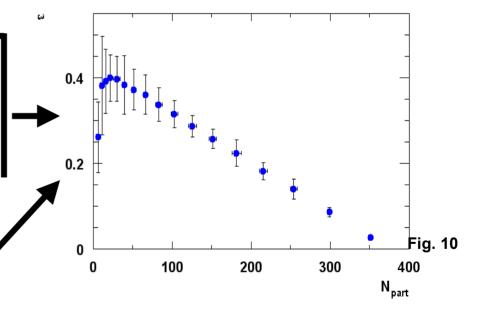
x

eccentricity

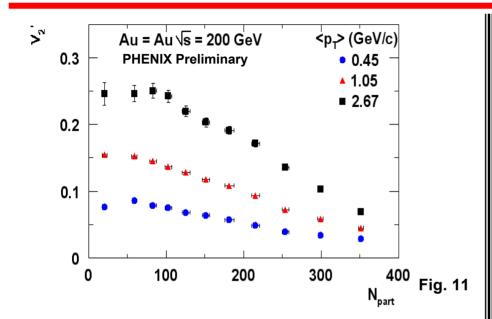
$$\varepsilon = \frac{\langle y^2 \rangle - \langle x^2 \rangle}{\langle y^2 \rangle + \langle x^2 \rangle}$$

 For eccentricity driven anisotropy, a rather specific centrality dependence is predicted. Namely, v<sub>2</sub> should follow the variation of eccentricity with N<sub>part</sub> and show eccentricity scaling.

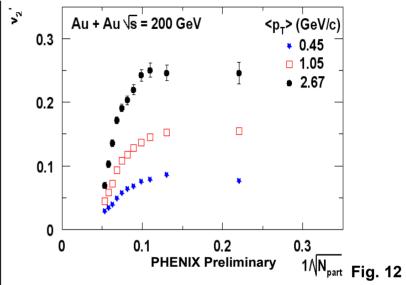
Variation of eccentricity with number of participants based on a Glauber model



#### Experimental Results (Test of eccentricity scaling)



•=> The centrality dependence observed for both high and low pT particles follow the same patterns which are strikingly similar to the expected dependence shown in Fig. 10.



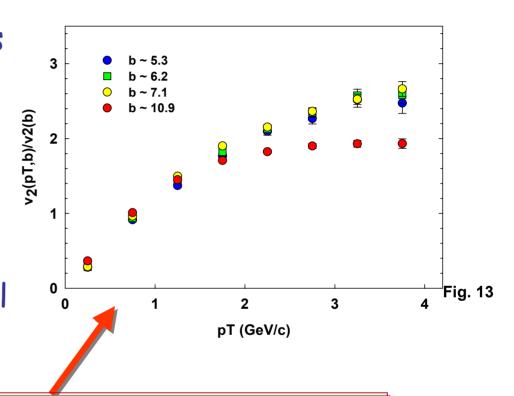
- Models based on minijet production predict that  $v_2$  should scale with  $1/\sqrt{Npart}$
- Fig. 12 indicates that the data is compatible with this scenario only for a limited range of centralities

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#### Experimental Results (Further Tests of eccentricity scaling)

If the initial eccentricity is a major driving force for the anisotropy. Then one expects approximate eccentricity scaling.

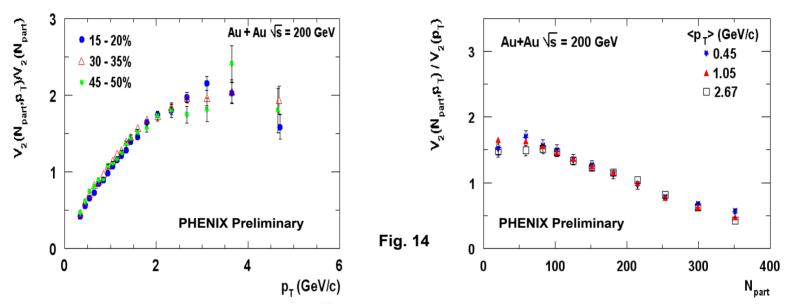
 Since the integral anisotropy is proportional to the eccentricity, one can scale by this integral



• This scaling [of the anisotropy] is observed for a broad range of centralities in the model of Molnar et al. (Nucl. Phys. A697, 495, 2002) if large opacities are assumed.

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#### Experimental Results (Tests of eccentricity scaling)



- The data indicates that the differential anisotropy scales with the integral anisotropy.
- Scaling property holds for both high and low p<sub>T</sub> particles. If jets dominate high pT particles then jet quenching could lead to the observed scaling for these particles.

The observed scaling property also suggest a factorization of the anisotropy.

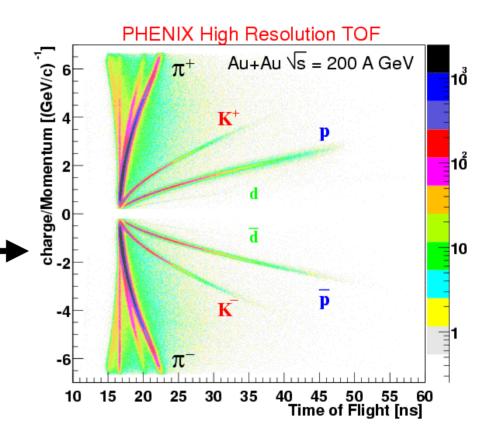
$$v_2(b,p_T) \approx v_2(b) v_2(p_T)$$

### **Ongoing analysis**

It is also important to study the flavor dependence of the anisotropy.

 Good particle identification is achieved in the PHENIX TOF and EMCAL respectively

Ongoing analyses focus on: measuring v<sub>2</sub> of identified hadrons using the TOF and Electromagnetic Calorimeter (EMCAL)



# **Summary / Conclusion**

- Detailed differential azimuthal anisotropy measurements have been made with PHENIX via cumulants of azimuthal correlations.
- These measurements indicate that:
  - ➤ High & low p<sub>T</sub> particles are correlated
  - v<sub>2</sub> is essentially independent of p<sub>T ref</sub>
  - $\triangleright$  v<sub>2</sub>(b,p<sub>T</sub>) factorizes in v<sub>2</sub>(b)v<sub>2</sub>(p<sub>T</sub>)
  - ➤ There appears to be eccentricity scaling of v<sub>2</sub> at high p<sub>T</sub>

These results are compatible with correlation of jets with the reaction plane, as would be expected from jet quenching